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## Description

This invention relates to an organic composite-plated steel sheet applied with a film coating and more particularly it relates to an organic composite-plated steel sheet easily applied with a film coating which is superior in press workability, spot weldability and electrodeposition property and especially high corrosion resistance.

Recently, demands for reduction of cost and improvement of corrosion resistance of zinc or zinc base alloy plated steel sheets for automobiles and household appliances have increased and research on new products has been widely made.

For example, weldable steel sheets comprising a basic steel sheet film-coated with an electrically conductive coating composition containing an electrically conductive metal powder are disclosed in Japanese Patent Kokai No. 61-23766 and Japanese patent Kokoku No. 62-20024. As a representative thereof, Zincrometal has been offered at markets. However, these suffer from practical problems such as dragging caused by press working and flaws formed by sticking of peeled film to mold, resulting in damages of appearance of pressed product.

Furthermore, improvement in corrosion resistance by application of an aqueous solution of a mixture of water-dispersible emulsion resin with a highly corrosion resistance chromic acid or a chromium compound onto the surface of zinc or zinc base alloy plated steel sheet are proposed in Japanese Patent Kokoku No. 55-51032 and Japanese Patent Kokai Nos. 59-162278 and 61-584. Although high in corrosion resistance, these sheets also have practical problems such as sweating and dissolving-out of chromium with aqueous treating solutions. Moreover, coating of a blend of water-dispersible emulsion resin and an organic composite silicate (silica sol, silane coupling agent) is proposed in Japanese Patent Kokai Nos. 60-50181 and 50-149786. According to these methods the problem caused by dissolving-out of chromium has been considerably improved, but since silica is contained as stable colloid, alkali ion or ammonium ion is present which also causes problems in properties of coating film, especially water resistance. Further, in case of solvent type coating compositions containing powdered silica, viscosity of coating composition increases very much due to its structural viscosity and coating in uniform film becomes impossible. The viscosity may be reduced by breaking the structural viscosity with hydrogen bond of alcohols, but this method cannot be applied to the system where polyisocyanate compounds are used as curing agent.

Thus, thin film-coated corrosion resistance steel sheets have been required to have (1) higher corrosion resistance, (2) higher adhesion to coating film (especially cation electrodeposited film) formed on the steel sheet and (3) lower baking temperature (140-170 °C) for improvement in working strength of the steel sheet. Various coating compositions have been proposed which can be expected to afford desirable results. However, since there is the problem of thixotropy in coating composition as mentioned above which is considered to be especially significant in the system where polyisocyanate compound is used as a curing agent, none of practically applicable coating compositions containing organic solvent-soluble epoxy resin, polyisocyanate compound and silica particle have been obtained as those for solvent type thin film-coated corrosion resistance steel sheets.

Accordingly, the principal object of this invention is to provide a weldable organic composite-plated steel sheet which causes no dissolving-out of harmful substances such as chromium during surface treatment by users and is high in corrosion resistance and workability and superior in electrodeposition coatability which are attained by thin film-coating at low baking temperatures.

This invention which aims at dissolving the above problems is an organic composite-plated steel sheet excellent in press workability, weldability, electrodeposition coatability and corrosion resistance which comprises a zinc plated, aluminum plated or zinc base composite alloy plated steel sheet as a substrate, an insoluble chromate film of 5% or less in the content of water-soluble matter formed at a coverage of 10-150 mg/m<sup>2</sup> in terms of total chromium content as a first layer on the surface of said substrate and a solid film of a coating composition having the following composition coated at a thickness of 0.3-5 μm on said first layer as a second layer:

- (A) at least 30% by weight, based on solid content of the composition, of a bisphenol type epoxy resin having a number-average molecular weight of 300-100,000,
- (B) at least one curing agent selected from the group consisting of a polyisocyanate compound and a block polyisocyanate compound at a weight ratio to the epoxy resin solid content of 1/10 - 20/10,
- (C) 5-50% by weight, based on solid content of the composition, of fumed silica having an average particle size of 0.1-100 mμ and
- (D) above 40% by weight, based on the weight of the composition, of a ketone organic solvent, the solid content in the composition being 10-50% by weight.

In the above coating composition, examples for the ketone organic solvent (D) can be methyl isobutyl

ketone, acetone, cyclohexanone and isophorone.

Further, the above coating composition may contain a resol type phenol resin at a weight ratio of 10/1 - 1/10 to solid content of the curing agent (B).

Besides, the coating composition may contain a polyethylene wax in an amount of 0.1-10% by weight of solid content of the composition.

This invention is characterized in combination of a plated steel sheet having thereon a specific chromate film with a film of an organic solvent type coating composition comprising a bisphenol type epoxy resin, a polyisocyanate compound, fumed silica and a ketone organic solvent which is coated on said steel sheet. That is, the coating composition is characterized by containing a polyisocyanate compound, if necessary, a blocked polyisocyanate compound for low temperature baking and containing micronized dry silica (fumed silica) in a high concentration for improvement of corrosion resistance. As a result of intensive research for realization of organic composite-plated steel sheet improved in properties such as spot weldability, electrodeposition coatability and press workability by thin film-coating of the above coating composition, this invention has been proposed. This invention has also been made based on the finding that viscosity of the coating composition can be effectively reduced by adding a ketone organic solvent to the system of bisphenol type epoxy resin/polyisocyanate curing composition/fumed silica and it is important to add the solvent together with a lubricant, if necessary, to adjust the solid content of the coating composition to 10-50% by weight.

The zinc plated, aluminum plated and zinc base composite alloy plated steel sheets used in this invention include, as electroplated steel sheets, zinc plated steel sheets, zinc-nickel alloy plated steel sheets, zinc-iron alloy plated steel sheets, and zinc base composite plated steel sheets plated with zinc-nickel or zinc-iron alloy in which a metal oxide such as  $\text{SiO}_2$ ,  $\text{TiO}_2$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{ZrO}_2$  or  $\text{BaCrO}_4$  is dispersed and, as hot dipping plated steel sheets, galvanized steel sheets, alloyed zinc steel sheets, zinc-aluminum plated steel sheets and aluminum plated steel sheets. These may be plated by conventional methods.

Effects of this invention will be explained below.

#### (1) Insoluble chromate film:

The chromate film used in this invention which is present between the under plating layer and the upper coating film is an important film in that it improves adhesion of the coating film, providing the resulting organic composite-plated steel sheet with high corrosion resistance. Especially, swelling and dissolving-out resistance against water is essential and thus the chromate film must be insoluble.

When water-soluble matter of the chromate film exceeds 5%, as mentioned above, chromium considerably dissolves out due to swelling of the chromate film and this causes deterioration in adhesion to the upper coating film and damages appearance of electrodeposited coating film (gas pinholes, etc.) and thus, it is difficult to further improve corrosion resistance. Furthermore, there often occur contamination of treating solution and complication of operation due to waste water disposal. The content of the water-soluble matter in the chromate film is preferably 3% or less.

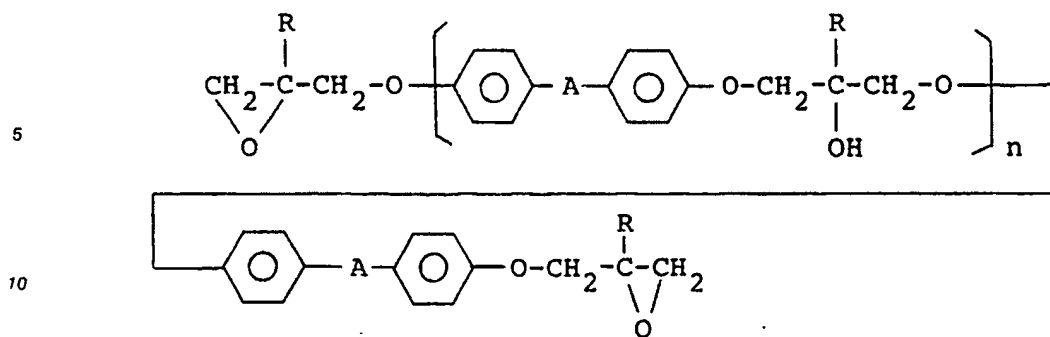
When deposition amount of the thus insoluble chromate film is less than 10 mg/m<sup>2</sup> in terms of total chromium amount, adhesion to the upper coating film is somewhat insufficient and it is difficult to further enhance corrosion resistance. When total chromium amount exceeds 150 mg/m<sup>2</sup>, adhesion to the upper coating film considerably decreases due to cohesive failure of chromate film by press working and further, problems occur in continuous spotting at spot welding.

Deposition amount of an insoluble chromate film is preferably 20-100 mg/m<sup>2</sup> in terms of total chromium amount.

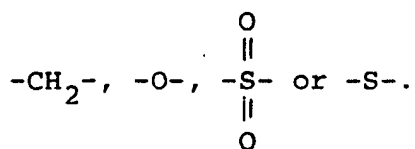
#### (2) Organic solvent type coating film:

As epoxy binder resin (A) used in formation of organic coating film according to this invention, there may be used bisphenol type epoxy resin which is organic solvent soluble, superior in water resistance and alkali resistance and especially superior in adhesion to base and to over coating film and has a number-average molecular weight of 300-100,000.

For example, the resin represented by the following formula may be used.



wherein R denotes H or CH<sub>3</sub> and -A- denotes >C(CH<sub>3</sub>)<sub>2</sub>,



When -A- is >C(CH<sub>3</sub>)<sub>2</sub> in the above formula, especially preferable result can be obtained. When the number-average molecular weight is less than 300, reaction does not provides sufficient polymerization and corrosion resistance of the coating film is unsatisfactory. On the other hand, when more than 100,000, also crosslinking reaction does not sufficiently proceed and similarly corrosion resistance of the coating film is insufficient.

Amount of the bisphenol type epoxy resin (A) must be 30% by weight or more based on the solid content of the coating composition. When less than 30% by weight, binding action of the resin for dry silica decreases and formation of coating composition becomes difficult and besides, the coating film is brittle, resulting in insufficient adhesion for working.

Next, curing agent (B) comprises a polyisocyanate compound and/or a block polyisocyanate compound.

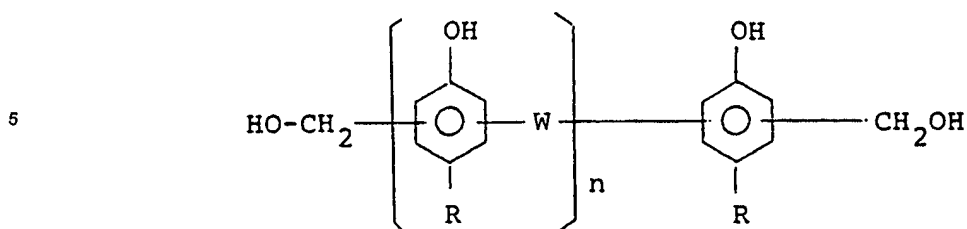
As the polyisocyanate compound, mention may be made of, for example, aliphatic or alicyclic diisocyanate compounds such as hexamethylene diisocyanate, isophorone diisocyanate and hydrogenated diphenylmethane diisocyanate, aromatic diisocyanate compounds such as tolylene diisocyanate and diphenylmethane-4,4'-diisocyanate, triisocyanate compounds such as adducts of 1 mol of trimethylolpropane and 3 mols of said diisocyanate and trimers of diisocyanate such as hexamethylene diisocyanate or tolylene diisocyanate. These may be used alone or in combination of two or more.

The block polyisocyanate compounds include, for example, said isocyanates blocked with a blocking agent. Such blocking agent must be such that the adduct produced by addition to isocyanate group is stable at room temperature and dissociates at baking of coating film to reproduce free isocyanate group.

As such blocking agents, mention may be made of, for example, lactam blocking agents such as  $\epsilon$ -caprolactam and  $\gamma$ -butyrolactam, oxime blocking agents such as methyl ethyl ketoxime and cyclohexanone oxime, alcohol blocking agents such as methanol, ethanol and isobutyl alcohol, phenol blocking agents such as phenol, p-tert-butyl phenol and cresol and ester blocking agents such as ethyl acetoacetate and methyl acetoacetate. Especially preferred are methyl ethyl ketoxime and ethyl acetoacetate which dissociate at a low temperature and are stable under the conditions of storage of coating composition.

Amount of the curing agent (B) is 1/10 - 20/10 at weight ratio to the solid content of the epoxy resin (A). At a low temperature and in a short time, (A) and (B) react to afford a suitable vehicle system. The reaction sufficiently proceeds, for example, at the highest temperature of the material to be coated of 160°C or lower and for a baking time of 5-60 seconds. When the mixing ratio (B)/(A) is less than 1/10, the crosslinking reaction proceeds insufficiently, resulting in reduction of corrosion resistance of the film. When it is more than 20/10, water resistance and alkali resistance of the coating film and besides adhesion to overcoating film are insufficient.

If necessary, a resol type phenolic resin can be added to the curing agent. This is effective for acceleration of film-forming reaction at low temperature baking (the highest temperature of sheet: about 100-130°C). Especially preferred is a resol type phenolic resin represented by the following formula:



10 wherein n is 0-4; W denotes  $-\text{CH}_2-$  or  $-\text{CH}_2-\text{O}-\text{CH}_2-$  and R denotes  $\text{CH}_3$ , H or



20 Addition amount of the resol type phenolic resin is preferably 10/1 - 1/10 at a weight ratio to the solid content of the curing agent (B). When the ratio is more than 10/1, alkali resistance decreases and is unsatisfactory and when less than 1/10, effect of acceleration of reaction is sometimes not recognized.

Further, in the present invention, fumed silica (C) having an average particle size of 0.1-100  $\mu\text{m}$  is used in an amount of 5-50% by weight of the solid content of the coating composition in order to impart high corrosion resistance without dissolving-out of harmful substances into degreasing and film treating bath. If the silica particle is less than 0.1  $\mu\text{m}$  in average particle size as primary particle, alkali resistance and adhesion to overcoating film are unsatisfactory. If it is more than 100  $\mu\text{m}$ , the corrosion resistance decreases and besides smoothness of electrodeposited coating film is deteriorated. Thus, the average particle size of the silica particle is within the range of 0.1-100  $\mu\text{m}$ , preferably 5  $\mu\text{m}$  - 40  $\mu\text{m}$ . The amount of the fumed silica (C) is suitably 5-50% by weight, preferably 15-30% by weight of the solid content of the coating composition. The addition of fumed silica (C) in such a large amount has become possible by use of the following ketone organic solvent (D). When the amount of the fumed silica is less than 5% by weight, corrosion resistance is insufficient and when more than 50% by weight, adhesion for working of coating film and spot weldability of the sheet are unsatisfactory and further the composition becomes highly viscous and is difficult to coat in a uniform thin film. Thus, the object of this invention cannot be sufficiently accomplished.

According to this invention, the above components are dissolved or dispersed in an organic solvent to obtain the coating composition. As the organic solvent, a ketone organic solvent (D) is added in an amount of at least 40% by weight of the coating composition and the composition is adjusted to 10-50% by weight in solid concentration. A uniform thin film can be easily formed from such composition. If the solid concentration of the coating composition is less than 10%, solvent content is too high and this is not economical and if more than 50%, uniform thin film is difficult to form and thus coating operability is inferior.

Especially suitable ketone organic solvents are, for example, methyl isobutyl ketone, acetone, cyclohexanone and isophorone. If necessary, other solvents may be used in combination, but solvents which react with polyisocyanate compounds such as water and alcohol should not be used.

Relation between the solvent used and the fumed silica will be explained. When the content of fumed silica based on solid matter in the coating composition is increased in order to ensure high corrosion resistance, viscosity of the coating composition becomes too high and the composition is apt to agglomerate and uniform coating of coating composition becomes difficult. Especially, it is almost impossible to form a uniform thin film (several microns). Hitherto, solvents high in hydrogen bonding such as water or alcohol solvents have been used to reduce the viscosity. However, these solvents have limitation in kinds of resins which they can dissolve and furthermore, isocyanate compounds cannot be used. Therefore, there is less degree of freedom in design for blending of coating compositions and it is difficult to obtain coating films of quality sufficient for attaining the object of this invention.

In this invention, as explained above, addition of fumed silica in high concentration has become possible by using ketone organic solvents and besides these solvents can stably dissolve the bisphenol type epoxy resin and polyisocyanate compound which can form rigid coating film at low temperatures. Thus, the object of this invention can be attained.

From the viewpoint of press workability of corrosion resistant steel sheet, the coating composition of this invention may contain lubricants such as carboxylic acid esters, metal salts of carboxylic acid and polyalkylene glycols in addition to polyolefins and furthermore lubricant powders such as molybdenum disulfide, silicon compounds and fluorine compounds. It is preferred to add these lubricants in an amount of 0.1-10% by weight of solid content of coating composition to make further improvement of workability. Especially preferred lubricant is a polyethylene wax having a molecular weight of 1,000-10,000 and an acid value of 15 mg/g KOH or less. When addition amount of this wax is less than 0.1% by weight, frictional resistance on the surface of coating film is high and dragging of mold and peeling of coating film occur during press working. When it is more than 10% by weight, shrinkage unevenness of the lubricants are produced in water cooling zone after baking of coating film. This often damages finished appearance of coat.

If acid value of the wax exceeds 15 KOH mg/g, the wax dissolves into coating film and so lubricating effect of the wax for the coating film decreases. Therefore, acid value must be 15 KOH mg/g or less and thus wax layer is formed on the surface of coating film and exhibits high lubricating effects. This wax layer is mainly formed in the depressed portions and these portions act as current-carrying points to prevent formation of gas pinholes or craters during cationic electrodeposition coating employed for coating of automobiles, resulting in stable production of beautiful electrodeposition appearance.

The amount of said lubricant added in the coating composition is preferably 0.3-3% by weight.

In this invention, when the thickness of coating film of the coating composition is less than 0.3  $\mu\text{m}$  as a solid film, corrosion resistance is not sufficient and when it is more than 5  $\mu\text{m}$ , difficulties occur in spot weldability and appearance of electrodeposited coating. Practically preferred range of thickness is 0.5-2  $\mu\text{m}$ .

In the organic composite-plated steel sheet of this invention, the coating composition which constitutes the organic solvent type coating film of the uppermost layer may contain the following pigments for further improvement of function of coating film. That is, rustproofing pigments such as chromate pigments, especially insoluble zinc, lead and barium salts, phosphate pigments and plumbate salt pigments, loading pigments such as carbonate pigments and silicate pigments, coloring pigments such as titanium oxide and carbon, rustproofing agents such as amine compounds, phenolic carboxylic acid and dispersion stabilizers. Considering spot weldability and press workability, the average particle size thereof is adjusted preferably to 10  $\mu\text{m}$  or less.

Baking conditions for coating film of the coating composition is not critical, but it is possible to carry out short time baking treatment with retention of good performances at final temperature of sheet at baking in a wide range of 100-200 °C.

Coating can be performed by any known methods such as roll coating method, curtain flow coating method and the like.

The organic composite-plated steel sheet of this invention has been markedly improved in press workability and spot weldability to remove the problems seen in these properties in the conventional sheets and has been further improved in electrodeposition coatability and corrosion resistance. This organic composite-plated steel sheet meets the requirements in the market.

This invention will be explained by the following examples in more detail.

#### Example

A low-carbon steel sheet of 0.8 mm thick was subjected to the zinc or zinc base composite alloy plating or aluminum plating as shown in Table 1 by known methods and immediately thereafter to the insoluble chromate treatment as shown in Table 1. Subsequently, the coating composition having the specific composition as shown in Table 1 was coated on one side at the given thickness by roll coating and immediately was subjected to baking treatment so that the highest temperature of the sheet reached 150 °C in 20 seconds. Performances of the thus coated steel sheets are shown in Table 1. Blending ratios of the components of the coating compositions are shown by % by weight. Effects of insoluble property and coverage (adhering amount) of the chromate film as an undercoat are shown in Examples 1-12 and Comparative Examples 13-15. It will be clear therefrom that the chromate film provided between the coating film and the under plating layer must be insoluble in water for improvements of various properties such as corrosion resistance. Further, it will be recognized that the range of coverage specified in this invention is preferred from the points of properties and cost.

Effects of the requirements in the coating composition in this invention will be explained.

First, proper molecular weight and blending ratio of the principal resin are shown by Examples 3 and 16-18, Comparative Examples 19-20 and Examples 21-24. From the results, it can be seen that epoxy resins are preferred as the principal resin and too high molecular weight thereof is not so effective for

corrosion resistance and press workability and preferred molecular weight is 4,000 or less. Furthermore, the amount of the principal resin is preferably 30-50% by weight.

Next, as shown in Examples 25-27 and 3 and Comparative Examples 28-29, hexamethylene diisocyanate base curing agents are preferred as curing agent for the resin and those which are blocked at isocyanate group (-NCO) with ethyl acetoacetate or  $\epsilon$ -caprolactam are desirable from the points of pot life of coating composition and coating operation. Further, it will be seen that the blending ratio of the curing agent is suitably 1-20, preferably 3-10 for 10 of the principal resin in order to obtain sufficient film strength by low temperature baking.

Fumed silica contained in coating film greatly contributes to obtaining high corrosion resistance of the organic composite-plated steel sheet of this invention and blending ratio and proper particle size are shown by Examples 3 and 30-38 and Comparative Examples 39-41. It can be seen therefrom that fumed silica of fine particles is preferred and water resistance and swelling resistance of coating film can be improved and high corrosion resistance can be attained by adding such fumed silica in an amount within the range as specified in this invention.

Next, with reference to the lubricant used in the coating film in this invention, examination was made mainly on polyethylene lubricant and the results are shown in Examples 3 and 42-47 and Comparative Examples 48-49. Even when no polyethylene lubricant was contained, there will be no practical problem in press workability (powdering), but in order to further decrease the frictional resistance of coating film to maintain faultless workability level without no possibility of dragging, it is preferred to add the lubricant in an amount as specified in this invention. Addition of the lubricant in too much amount causes reduction of water swelling resistance of coating film resulting in deterioration of corrosion resistance.

Results of investigation on proper organic solvents in coating film are shown in Examples 3 and 50 and Comparative Examples 51-52.

As organic solvents used in this invention, ketone solvents may be used alone or in admixture. However, water or alcohol solvents which are poor in compatibility with polyisocyanate curing agents and cause difficulties in coating operation and quality should not be used.

Proper thickness of coating film is investigated in Examples 53-59 and Comparative Examples 60-61. As is clear from the results, the range as specified in this invention is necessary to employ in view of corrosion resistance and spot weldability. Results obtained when kind of the under plating layer is changed are shown in Examples 62-76, from which it will be recognized that this invention can be applied to various under plating layers deposited on steel sheets.

As explained above, the organic composite-plated steel sheet of this invention which comprises an under plated steel sheet, a first layer of a special insoluble chromate film provided on said under plating layer and a second layer of a specific coating composition having a specific thickness as a solid film provided on said first layer has markedly improved corrosion resistance, press workability, electrodeposition coatability, chromium dissolving-out resistance and spot weldability and this steel sheet sufficiently meets the demands of users. Furthermore, baking of coating film at low temperatures also become possible and thus deterioration of material of base can also be overcome. Such are unexpected results.

Chemicals and methods of evaluation used in the examples and comparative examples given in Table 1 are as shown in the notes after Table 1.

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Table I

	No.	Plating *1		Chromate *2	
		Kind	Amount (g/m <sup>2</sup> )	Content of water soluble matter (%)	Coverage T.Cr <sub>2</sub> (mg/m <sup>2</sup> )
Example	1	Electroplating of Zn-Ni alloy	20	0	40
"	2	"	"	0.3	"
"	3	"	"	0.5	"
"	4	"	"	1.0	"
"	5	"	"	3.0	"
"	6	"	"	5.0	"
"	7	"	"	0.5	10
"	8	"	"	"	20
"	9	"	"	"	60
"	10	"	"	"	100



Organic solvent type coating film

9

Table I (Continued)

Organic solvent type coating film			Performances *8			
Kind	Organic solvent		*7 Thickness of coating film ( $\mu\text{m}$ )	Press workability	Spot weldability	Electrodeposition coatability
	Blending ratio (%)					Appearance Adhesion
Cyclohexanone	55.2		1.0	◎	◎	◎
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"
"	"		"	"	"	"

Table I (Continued)

Performances *8		
Corrosion resistance	Adhesion of coating film	Dissolving-out of chromium
◎	◎	◎
"	"	"
"	"	"
"	"	"
"	"	"
"	"	"
"	"	"
"	"	"
"	"	"
"	"	"
"	"	"
"	"	"

Table I (Continued)

Example	11	Electroplating of Zn-Ni alloy	20	0.5	120
"	12	"	"	"	150
Comparative Example	13	"	"	10.0	40
"	14	"	"	0.5	5
"	15	"	"	"	200
Example	16	"	"	"	40
"	17	"	"	"	"
"	18	"	"	"	"
Comparative Example	19	"	"	"	"
"	20	"	"	"	"
Example	21	"	"	"	"
"	22	"	"	"	"
"	23	"	"	"	"
"	24	"	"	"	"

Table I (Continued)

Epoxy	2900	48.7	HMDI-AEA	5/10	AEROSIL 300 8	25	2
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	470	"	"	"	"	"	"
"	1000	"	"	"	"	"	"
"	3750	"	"	"	"	"	"
Oil free polyester	15000	"	"	"	"	"	"
Carboxylated polyethylene	100000	75.0	-	-	SNOWTEX N 10 - 20	"	-
Epoxy	2900	66.4	HMDI-AEA	1/10	AEROSIL 300 8	"	2
"	"	56.2	"	3/10	"	"	"
"	"	39.4	"	10/10	"	"	"
"	"	33.2	"	12/10	"	"	"

Table I (Continued)

Cyclohexanone	55.2	1.0	⊙	⊙	⊙	⊙	⊙
"	"	"	"	"	"	"	⊙
"	"	"	"	"	"	Δ	Δ
"	"	"	○	"	"	⊙	○
"	"	"	Δ - ○	Δ	Δ	○	Δ - ○
"	"	"	⊙	⊙	⊙	⊙	⊙
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	○
Water	80	"	x	"	"	"	x
Cyclohexanone	49.7	"	⊙	"	"	"	⊙
"	52.9	"	"	"	"	"	"
"	59.1	"	"	"	"	"	"
"	60.1	"	"	"	"	"	"

Table I (Continued)

5														
	⊙	"	x	⊙	⊙ - ○	⊙	"	"	"	"	"	"	"	"
10														
	⊙	"	Δ	Δ	Δ - ○	⊙	"	"	"	"	"	"	"	"
15														
	⊙	"	○	x - Δ	○ - ⊙	⊙	"	"	x	"	⊙	"	"	"
20														
25														
30														
35														
40														
45														
50														
55														

Table I (Continued)

Example	25	Electroplating of Zn-Ni alloy	20	0.5	40
"	26	"	"	"	"
"	27	"	"	"	"
Comparative Example	28	"	"	"	"
"	29	"	"	"	"
Example	30	"	"	"	"
"	31	"	"	"	"
"	32	"	"	"	"
"	33	"	"	"	"
"	34	"	"	"	"
"	35	"	"	"	"
"	36	"	"	"	"



Table I (Continued)

Epoxy	2900	48.7	HMDI	5/10	AEROSIL 300 8	25	2
"	"	"	HMDI-CLN	"	"	"	"
"	"	"	HMDI-AEA 3 BKS 316 2	5/10	"	"	"
"	"	60.8	SUPER- BECKAMINE	2/10	"	"	"
"	"	"	BKS-316	"	"	"	"
"	"	62.1	HMDI-AEA	5/10	"	5	"
"	"	58.7	"	"	"	10	"
"	"	55.3	"	"	"	15	"
"	"	42.0	"	"	"	35	"
"	"	35.4	"	"	"	50	"
"	"	48.7	"	"	AEROSIL 300 0.1	25	"
"	"	"	"	"	" 1	"	"

Table I (Continued)

Cyclohexanone	56.7	1.0	⊙	⊙	⊙	⊙
"	"	"	"	"	"	⊙
"	54.2	"	"	"	"	"
"	47.7	"	○	"	"	⊙ - ○
"	50.2	"	"	"	"	○
"	50.5	"	⊙	"	"	⊙
"	53.0	"	"	"	"	"
"	52.5	"	"	"	"	"
"	57.5	"	"	"	"	"
"	59.8	"	"	"	"	"
"	55.2	"	"	"	"	"
"	"	"	"	"	"	"

Table I (Continued)

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⊙	"	"	"	"	"	"	"	"	"	"	"
⊙	"	"	○	"	⊙	"	"	"	"	"	"
⊙	"	"	○	"	⊙	"	"	"	"	"	"

Table I (Continued)

Example	37	Electroplating of Zn-Ni alloy	20	0.5	40
"	38	"	"	"	"
Comparative Example	39	"	"	"	"
"	40	"	"	"	"
"	41	"	"	"	"
Example	42	"	"	"	"
"	43	"	"	"	"
"	44	"	"	"	"
"	45	"	"	"	"
"	46	"	"	"	"
"	47	"	"	"	"
Comparative Example	48	"	"	"	"

Table I (Continued)

Epoxy	2900	48.7	HMDI-AEA	5/10	AEROSIL 300 40	25	2
"	"	"	"	"	" 100	"	"
"	"	"	"	"	Silica powder 1000	"	"
"	"	63.3	"	"	AEROSIL 300 8	3	"
"	"	28.7	"	"	"	55	"
"	"	48.7	"	"	"	25	0.1
"	"	"	"	"	"	"	0.5
"	"	"	"	"	"	"	1
"	"	"	"	"	"	"	3
"	"	"	"	"	"	"	5
"	"	"	"	"	"	"	10
"	"	"	"	"	"	"	0

Table I (Continued)

Cyclohexanone	55.2	1.0	⊙	⊙	⊙	⊙	⊙
"	"	"	"	"	"	"	"
"	"	"	x	Δ - ○	○	○	○
"	49.3	"	⊙	○	○	⊙	⊙
"	63.3	"	x	x - Δ	○	○	Δ
"	55.2	"	⊙	⊙	⊙	⊙	⊙
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	○	"	○ - Δ	○ - Δ	"

Table I (Continued)

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⊙	"	"	"	"	"	"	"	"	"	"	"
⊙	"	Δ - ○	⊙	x	⊙	"	"	"	"	"	"
⊙	"	x	x	○	⊙	"	"	"	"	"	○ - Δ

Table I (Continued)

49	Electroplating of Zn-Ni alloy	20	0.5	40
Comparative Example				
Example	"	"	"	"
Comparative Example	"	"	"	"
"	"	"	"	"
Example	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
"	"	"	"	"
Comparative Example	"	"	"	"



Table I (Continued)

	Epoxy	2900	48.7	HMDI-AEA	5/10	AEROSIL 300 8	25	15
5	"	"	"	"	"	"	"	2
10	"	"	"	"	"	"	"	"
15	"	"	"	"	"	"	"	"
20	"	"	"	"	"	"	"	"
25	"	"	"	"	"	"	"	"
30	"	"	"	"	"	"	"	"
35	"	"	"	"	"	"	"	"
40	"	"	"	"	"	"	"	"
45	"	"	"	"	"	"	"	"
50	"	"	"	"	"	"	"	"

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Table I (Continued)

Δ	⊙	⊙	⊙
⊙	"	"	"
(Coating was impossible due to high viscosity)			
Δ	x	⊙	⊙
⊙	⊙	"	"
"	"	"	"
"	"	"	"
"	"	"	"
"	"	"	"
"	"	"	"
"	"	"	"
"	"	"	"
Δ	"	"	"

Table I (Continued)

Comparative Example	61	Electroplating of Zn-Ni alloy	20	0.5	40
Example	62	Electroplating of Zn-Fe alloy	90	"	"
"	63	"	20	"	"
"	64	Electroplating of dispersion type alloy Zn-Ni-SiO <sub>2</sub>	20	"	"
"	65	Electroplating of dispersion type alloy Zn-Fe-SiO <sub>2</sub>	20	"	"
"	66	Electroplating of dispersion type alloy Zn-Fe-TiO <sub>2</sub>	30	"	"
"	67	Electroplating of dispersion type alloy Zn-Fe-Al <sub>2</sub> O <sub>3</sub>	20	"	"
"	68	Electroplating of dispersion type alloy Zn-Fe-Cr-ZrO <sub>2</sub>	"	"	"
"	69	Electroplating of dispersion type alloy Zn-Fe-Cr-SiO <sub>2</sub>	29	"	"
"	70	Hot dip galvannealing of Zn-Fe alloy	60	"	"
"	71	Hot dip plating of Zn-5Al alloy	60	"	"

Table I (Continued)

[illegible]

Table I (Continued)

Cyclohexanone	55.2	10.0	⊙	x	x - ○	⊙
"		1.0	"	⊙	⊙	⊙
"	"	"	"	"	"	"
"	"	"	"	"	"	"
"	"	"	"	"	"	"
"	"	"	"	"	"	"
"	"	"	"	"	"	"
"	"	"	"	"	"	"
"	"	"	"	"	"	"
"	"	"	"	"	"	"
"	"	"	"	"	"	"

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Table I (Continued)

⊙	"	"	"	"	"	"	"	"	"	"
⊙	"	"	"	"	"	"	"	"	"	"
⊙	"	"	"	"	"	"	"	"	"	"

Table I (Continued)

Example	72	Hot dip plating of Zn-5Al-0.1 Mg alloy	60	0.5	40
"	73	Electroplating of Zn-Fe alloy in two layers	20	"	"
"	74	Hot dip plating of Zn-5.5 Al-0.1 Si	60	"	"
"	75	Hot dip aluminizing	60	"	"
"	76	Hot dip galvanizing Zn	60	"	"



Table I (Continued)

Epoxy	2900	48.7	HMDI-AEA	5/10	AEROSIL 300 8	25	2
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"
"	"	"	"	"	"	"	"

Table I (Continued)

5	⊙	"	"	"	"
10	⊙	"	"	"	"
15	⊙	"	"	"	"
20	⊙	"	"	"	"
25	⊙	"	"	"	"
30	1.0	"	"	"	"
35	55.2	"	"	"	"
40	Cyclohexanone	"	"	"	"
45		"	"	"	"
50		"	"	"	"
55		"	"	"	"

Table I (Continued)

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⊙	=	=	=	=
⊙	=	=	=	=
⊙	=	=	=	=

Notes:

\*1: Measurement of amount deposited is in accordance  
with JIS H-0401.

\*2: Content of water soluble matter is shown by the  
ratio of difference in chromium deposition amount before  
and after dipping in boiling distilled water for 30  
minutes and initial deposited amount. Fluorescent X-ray  
analysis is used.

\*3: Type and molecular weight of main resins. (Blend-  
ing ratio is shown by % by weight for solid content of  
coating composition.)

EPIKOAT 1001 (Bisphenol type epoxy resin  
supplied by Shell Chemical Co.) ----- Molecular  
weight 900.

EPIKOAT 1007 (Bisphenol type epoxy resin  
supplied by Shell Chemical Co.) ----- Molecular  
weight 2900.

EPIKOAT 1009 (Bisphenol type epoxy resin  
supplied by Shell Chemical Co.) ----- Molecular  
weight 3750.

BYRON 200 (Oil free polyester resin supplied  
by Toyobo Co. Ltd.) ----- Molecular weight  
15000

Carboxylated polyethylene resin (carboxyl  
group 12 mol%, in the form of 20% aqueous  
solution)

\*4: Curing agent (Blending ratio is shown by % by weight  
for solid content of the coating composition.)

(Trimmer type)

HMDI: Hexamethylene diisocyanate

HMDI-AEA: Blocked ethyl acetoacetate.

HMDI-CLN: Blocked  $\epsilon$ -caprolactam.

SUPERBECKAMINE J-820-60 (melamine resin 60%

supplied by Dainippon Ink & Chemicals Inc.)

(for comparative examples). Phenolic resin

BKS-316 (Resol type phenolic resin supplied

by Showa Kobunshi Co.)

\*5: Fumed silica (Blending ratio is shown by % by weight for solid content of the coating composition.).

AEROSIL 300 (Japan Aerosil Co.) ----- average

particle size 8  $\mu$

AEROSIL OX50 (Japan Aerosil Co.) ----- average

particle size 40  $\mu$

SNOWTEX N (Nissan Chemical Industries, Ltd.)

in the form of 20% aqueous colloidal silica

solution.

\*6: Polyethylene was (Blending ratio is shown by % by weight for solid content of the coating composition.)

SERIDUST 3620 (Hoechst Co.) ----- Density:

0.95-0.97, Molecular weight: 2000 and Acid

value: 0.

\*7: Weight method: This is calculated from difference between initial weight of uncoated steel sheet and weight of the same steel sheet on which the coating composition is coated and dried.

\*8: Performance test methods

*EPIKDAT, BYRON, SUPER BECKAMINE, AEROSIL, SNOWTEX and SERIDUST are registered trade marks.*

(1) Press workability:

Sheet is subjected to cylindrical drawing (without coating oil) and thereafter, the surface of the worked portion on die side is subjected to peeling test by adhesive cellophane tape and the workability is evaluated by the following four gradings.

① : No peeling occurred.

- : A few dragging occurred with no peeling.
- △ : A slight powdering occurred.
- x : Considerable powdering and peeling occurred.

## (2) Spot weldability (continuous spotting):

This is measured using a copper electrode having a tip diameter of 6 mm with a pressing force of 200 kg\*f and a current of 8-9 KA at 10 cycles and evaluated by the following four gradings.

- ⊙ : Continuously 5000 or more spottings.
- : Continuously 4000 or more spottings.
- △ : Continuously 2000 or more spottings.
- x : Continuously less than 2000 spottings.

## (3) Electrodeposition coatability:

After phosphoric acid treatment (PB3020 supplied by Japan Parkerizing Co.), cation electrodeposition was conducted with POWERTOP U-100 (supplied by Nippon Paint Co., Ltd.) at 20 μm.

(i) Appearance: Presence of gas pinholes and craters is examined and evaluated by the following gradings.

- ⊙ : No defects occurred.
- : A few gas pinholes occurred.
- △ : Gas pinholes occurred partially.
- x : Gas pinholes occurred on the whole surface.

(ii) Adhesion: The sheet is dipped in a warm water of 40° C for 10 days and then 100 squares of 1 mm x 1 mm are cut on the surface. This surface is subjected to peeling test by adhesive tape. The adhesion is evaluated by the following gradings.

- ⊙ : No peeling occurred.
- : Slight peeling occurred.
- △ : Partial peeling occurred.
- x : Considerable peeling occurred.

(4) Corrosion resistance: This is evaluated by salt spray test (JIS Z-2371) of 2000 hours with a sheet having 1/2 crosscut.

- ⊙ : White rust of less than 10%
- : White rust of less than 30%
- △ : Red rust of less than 5%
- x : Red rust of more than 5%

(5) Adhesion of coating film: Secondary adhesion is evaluated by dipping the sheet with coating film in a boiling water for 4 hours, cutting 100 squares of 1 mm x 1 mm on the surface and subjecting the surface to peeling test by adhesive tape.

- ⊙ : No peeling occurred.
- : Slight peeling occurred.
- △ : Partial peeling occurred.
- x : Peeling occurred on the whole surface.

(6) Dissolving-out of chromium: The sheet is degreased with alkali (spray treatment with degreasing solution containing 20 g/l of L-4410 supplied by Japan Parkerizing Co. at 60° C for 5 minutes) and then total amount of chromium dissolving out into the degreasing solution is measured.

- ⊙ : Up to 5 mg/m<sup>2</sup>.
- : Up to 10 mg/m<sup>2</sup>.
- △ : Up to 30 mg/m<sup>2</sup>.
- x : More than 30 mg/m<sup>2</sup>.

## Claims

1. A steel sheet having an organic composite plating layer which comprises a steel sheet plated with zinc, aluminium or a composite electroplated and hot dipped plated layer on the basis of a zinc alloy, a chromate film as a first layer and a film comprising organic compounds as a second layer, characterized in that the first layer is an insoluble chromate film of 5% or less in content of water-soluble matter formed on the surface of said plated steel sheet at a coverage of 10-150 mg/m<sup>2</sup> in terms of total chromium content, and the second layer is obtained after coating the following composition at a thickness of 0.3-5 μm as a solid film on said first layer and baking them :
  - (A) a bisphenol type epoxy resin having a number-average molecular weight of 300-100,000 in an amount of 30% by weight or more based on solid content in the coating composition,

(B) at least one polyisocyanate compound and/or block polyisocyanate compound as a curing agent at a weight ratio to solid content in the epoxy resin of 1/10 - 20/10,

(C) fumed silica having an average particle size of 0.1 - 100  $\mu\text{m}$  in an amount of 5-50% by weight based on solid content in the coating composition, and

5 (D) a ketone organic solvent in an amount of 40% by weight or more of the coating composition, and the solid content in the coating composition being 10-50% by weight.

2. A steel sheet according to claim 1 wherein the ketone organic solvent (D) is methyl isobutyl ketone, acetone, cyclohexanone and/or isophorone.

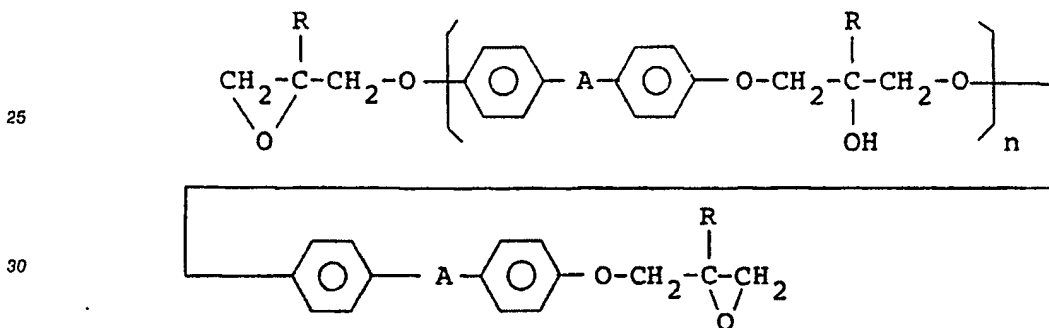
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3. A steel sheet according to claim 1 wherein the coating composition additionally contains a resol type phenolic resin at a weight ratio to solid content type phenolic resin at a weight ratio to solid content of the curing agent (B) in the epoxy resin of 10/1 - 1/10.

15 4. A steel sheet according to claim 1 wherein the coating composition additionally contains a polyethylene wax in an amount of 0.1-10% by weight based on solid content of the coating composition.

5. A steel sheet according to claim 1 wherein the bisphenol type epoxy resin (A) is represented by the following formula:

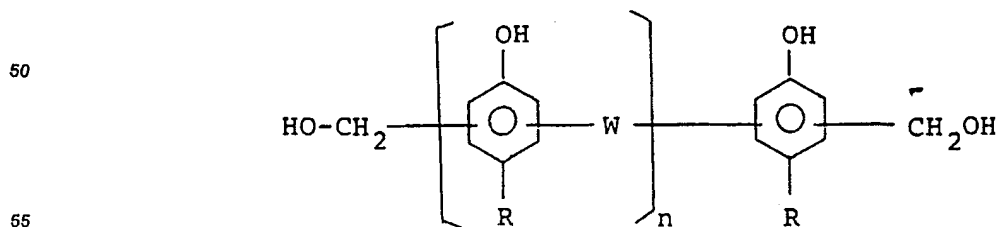
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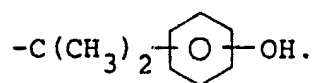
35 wherein R represents H or  $\text{CH}_3$  and -A- represents  $>\text{C}(\text{CH}_3)_2$ ,  $-\text{CH}_2-$ ,  $-\text{O}-$ ,



45 6. A steel sheet according to claim 3 wherein the resol type phenolic resin is represented by the following formula:



wherein n represents 0-4, W represents  $-\text{CH}_2-$  or  $-\text{CH}_2-\text{O}-\text{CH}_2-$  and R represents  $\text{CH}_3$ , H or



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7. A steel sheet according to claim 4 wherein the polyethylene wax has an acid value of 15 KOH mg/g or less.
- 10 8. A method for making a steel sheet according to claim 1 which comprises plating a steel sheet with zinc, aluminum or zinc base composite alloy, forming thereon an insoluble chromate film of 5% or less in content of water-soluble matter at a coverage of 10-150 mg/m<sup>2</sup> in terms of total chromium content, coating thereon in the form of a thin film a coating composition having the following composition at a thickness of 0.3 - 5 μm as a solid film and then baking the coating film:
- 15 (A) a bisphenol type epoxy resin having a number-average molecular weight of 300-100,000 in an amount of 30% by weight or more based on solid content in the coating composition,
- (B) at least one polyisocyanate compound or block polyisocyanate compound as a curing agent at a weight ratio to solid content in the epoxy resin of 1/10 - 20/10,
- (C) fumed silica having an average particle size of 0.1 - 100 mμ in an amount of 5-50% by weight
- 20 based on solid content in the coating composition, and
- (D) a ketone organic solvent in an amount of 40% by weight or more of the coating composition, and the solid content of the coating composition being 10-50% by weight.

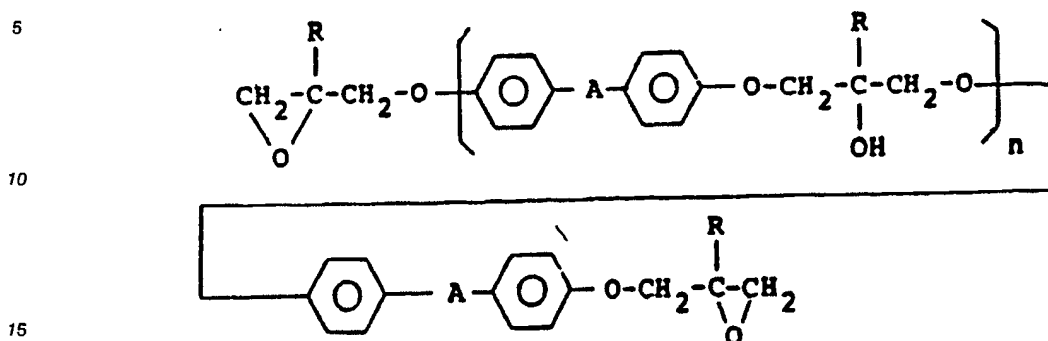
#### Revendications

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1. Tôle d'acier présentant une couche de revêtement en matériau composite organique qui comprend une tôle d'acier revêtue de zinc, d'aluminium ou d'un matériau composite métallisé par galvanisation et d'une couche de revêtement galvanisée par immersion à chaud à base d'un alliage de zinc, une pellicule chromée comme première couche et une pellicule comprenant des composés organiques
- 30 comme seconde couche, caractérisée en ce que la première couche est une pellicule chromée insoluble présentant une teneur de 5 % ou moins en matières solubles dans l'eau, formée sur la surface de ladite tôle d'acier revêtue en une application de 10 à 150 mg/m<sup>2</sup> pour ce qui est de la teneur totale en chrome, et en ce que la seconde couche est obtenue après revêtement de ladite première couche par une composition, sous forme d'une pellicule solide d'une épaisseur de 0,3 à 5 mμ et par cuisson, cette composition comprenant :
- 35 (A) une résine époxy de type bisphénol ayant un poids moléculaire moyen de 300 à 100 000, en une quantité de 30 % en poids ou plus, basée sur la teneur en solides dans la composition de revêtement,
- (B) au moins un composé polyisocyanate et/ou un composé polyisocyanate en bloc comme agent
- 40 de polymérisation, selon un rapport en poids avec la teneur en solides dans la résine époxy de 1/10 à 20/10,
- (C) de la silice fumée ayant une taille moyenne de particules de 0,1 à 100 mμ, en une quantité de 5 à 50 % en poids basée sur la teneur en solides dans la composition de revêtement, et
- (D) un solvant organique de type cétone en une quantité de 40 % en poids ou plus de la
- 45 composition de revêtement,
- la teneur en solides dans la composition de revêtement étant de 10 à 50 % en poids.
2. Tôle d'acier selon la revendication 1 dans laquelle le solvant organique du type cétone (D) est la méthyl isobutyl cétone, l'acétone, la cyclohexanone et/ou l'isophorone.
- 50 3. Tôle d'acier selon la revendication 1 dans laquelle, la composition de revêtement comprend en outre, une résine phénolique de type résol selon un rapport en poids avec la teneur en solides de l'agent de polymérisation (B) dans la résine époxy de 10/1 à 1/10.
4. Tôle d'acier selon la revendication 1 dans laquelle la composition de revêtement contient en outre une cire de polyéthylène selon une quantité de 0,1 à 10 % en poids basée sur la teneur en solides de la composition de revêtement.

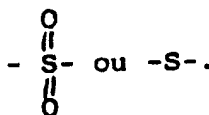


5. Tôle d'acier selon la revendication 1 dans laquelle la résine époxy de type bisphénol (A) est représentée par la formule suivante :



dans laquelle R représente H ou CH<sub>3</sub> et -A- représente >C(CH<sub>3</sub>)<sub>2</sub>-, -CH<sub>2</sub>-, -O-,

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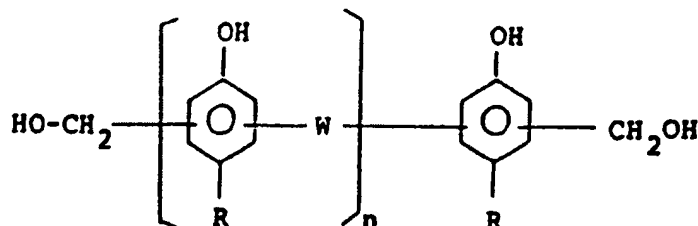


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6. Tôle d'acier selon la revendication 3 dans laquelle la résine phénolique de type résol est représentée par la formule suivante :

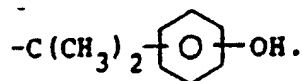
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dans laquelle n varie de 0 à 4, W représente -CH<sub>2</sub>- ou -CH<sub>2</sub>-O-CH<sub>2</sub>- et R représente CH<sub>3</sub>, H ou



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7. Tôle d'acier selon la revendication 4 dans laquelle la cire de polyéthylène présente un indice d'acidité de 15 KOH mg/g ou moins.

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8. Procédé de fabrication d'une tôle d'acier selon la revendication 1 qui consiste à revêtir une tôle d'acier avec du zinc, de l'aluminium ou un alliage composite à base de zinc, à former sur celle-ci une pellicule chromée insoluble présentant une teneur de 5 % ou moins en matières solubles dans l'eau, en une application de 10 à 150 mg/m<sup>2</sup> pour ce qui est de la teneur totale en chrome, à recouvrir celle-ci d'une fine pellicule d'une composition de revêtement sous forme d'une pellicule solide d'une épaisseur de 0,3 à 5 µm et en cuisant ensuite la pellicule de revêtement, cette composition comprenant :

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(A) une résine époxy de type bisphénol ayant un poids moléculaire moyen de 300 à 100 000, en une quantité de 30 % en poids ou plus, basée sur la teneur en solides dans la composition de revêtement,

(B) au moins un composé polyisocyanate et/ou un composé polyisocyanate en bloc comme agent de polymérisation, selon un rapport de poids avec la teneur en solides dans la résine époxy de 1/10 à 20/10,

(C) de la silice fumée ayant une taille moyenne de particules de 0,1 à 100 mμ, en une quantité de 5 à 50 % en poids basée sur la teneur en solides dans la composition de revêtement, et

(D) un solvant organique de type cétone, en une quantité de 40 % en poids ou plus de la composition de revêtement,

la teneur en solides de la composition de revêtement étant de 10 à 50 % en poids.

#### 10 Patentansprüche

1. Stahlblech mit einem organischen Verbundüberzug, umfassend ein Stahlblech, überzogen mit Zink, Aluminium oder einer Verbundschicht auf der Basis einer Zinklegierung, die galvanisiert und heißgetaucht wurde, einen Chromatfilm als erste Schicht und einen organische Verbindungen enthaltenden Film als eine zweite Schicht, **dadurch gekennzeichnet, daß**

die erste Schicht ein unlöslicher Chromatfilm mit 5 % oder weniger Gehalt an wasserlöslichen Stoffen ist, gebildet auf der Oberfläche des beschichteten Stahlbleches in einer Bedeckung von 10 bis 150 mg/m<sup>2</sup>, bezogen auf den Gesamtchromgehalt, und

die zweite Schicht, nach dem Auftragen der nachstehenden Zusammensetzung in einer Dicke von 0,3 bis 5 μm als ein fester Film auf der ersten Schicht und deren Ausheizen erhalten wird:

(A) ein Epoxidharz vom Bisphenoltyp mit einem Zahlenmittel-Molekulargewicht von 300 bis 100 000 in einer Menge von 30 Gew.-% oder mehr, bezogen auf den Feststoffgehalt im Überzug,

(B) mindestens eine Polyisocyanatverbindung und/oder eine Blockpolyisocyanatverbindung als Härter in einem Gewichtsverhältnis zum Feststoffgehalt im Epoxidharz von 1/10 bis 20/10,

(C) pyrogene Kieselsäure mit einer durchschnittlichen Teilchengröße von 0,1 bis 100 mμ in einer Menge von 5 bis 50 Gew.-%, bezogen auf den Feststoffgehalt im Überzug und

(D) ein organisches Lösungsmittel vom Ketontyp in einer Menge von 40 Gew.-% oder mehr, bezogen auf den Überzug,

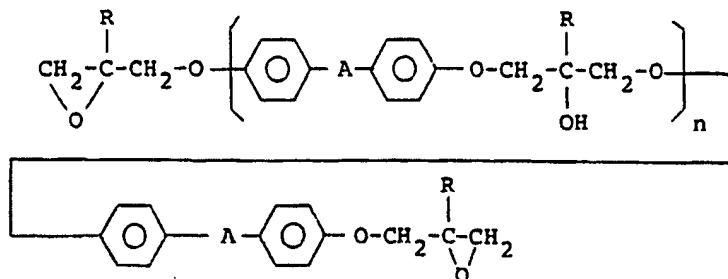
wobei der Feststoffgehalt im Überzug 10 bis 50 Gew.-% beträgt.

2. Stahlblech nach Anspruch 1, wobei das organische Lösungsmittel (D) vom Ketontyp Methylisobutylketon, Aceton, Cyclohexanon und/oder Isophoron ist.

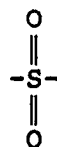
3. Stahlblech nach Anspruch 1, wobei der Überzug zusätzlich ein Phenolharz von Resoltyp im Gewichtsverhältnis zum Feststoffgehalt des Härters (B) im Epoxidharz von 10/1 bis 1/10 enthält.

4. Stahlblech nach Anspruch 1, wobei der Überzug zusätzlich ein Polyethylenwachs in einer Menge von 0,1 bis 10 Gew.-%, bezogen auf den Feststoffgehalt des Überzugs, enthält.

5. Stahlblech nach Anspruch 1, wobei das Epoxidharz (A) vom Bisphenoltyp die nachstehende Formel aufweist:

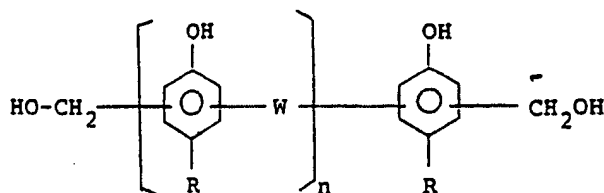


in der R ein Wasserstoffatom oder eine Methylgruppe darstellt und -A- die Gruppe  $>\text{C}(\text{CH}_3)_2$ ,  $-\text{CH}_2-$ ,  $-\text{O}-$ ,

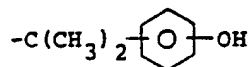


oder -S- bedeutet.

6. Stahlblech nach Anspruch 3, wobei das Phenolharz vom Resoltyp die nachstehende Formel hat:



in der n durch die Zahlen 0 bis 4 wiedergegeben wird, W die Gruppe  $-\text{CH}_2-$  oder  $-\text{CH}_2-\text{O}-\text{CH}_2-$  darstellt und R eine Methylgruppe, ein Wasserstoffatom oder die Gruppe



bedeutet.

7. Stahlblech nach Anspruch 4, wobei das Polyethylenwachs eine Säurezahl von 15 KOH mg/g oder weniger besitzt.
8. Verfahren zur Herstellung eines Stahlblechs gemäß Anspruch 1, umfassend den Überzug eines Stahlbleches mit Zink, Aluminium oder einer Verbundlegierung auf Zinkbasis, Herstellen eines unlöslichen Chromatfilmes darauf mit 5 % oder weniger Gehalt an wasserlöslichen Stoffen in einer Bedekung von 10 bis 150 mg/m<sup>2</sup>, bezogen auf den Gesamtchromgehalt, Auftragen eines Überzugs mit der nachstehenden Zusammensetzung in Form eines dünnen Filmes in einer Dicke von 0,3 bis 5 µm als einen festen Film darauf und Ausheizen des aufgetragenen Filmes:

(A) ein Epoxidharz vom Bisphenoltyp mit einem Zahlenmittel-Molekulargewicht von 300 bis 100 000 in einer Menge von 30 Gew.-% oder mehr, bezogen auf den Feststoffgehalt im Überzug,

(B) mindestens eine Polyisocyanatverbindung und/oder eine Blockpolyisocyanatverbindung als Härter in einem Gewichtsverhältnis zum Feststoffgehalt im Epoxidharz von 1/10 bis 20/10,

(C) pyrogene Kieselsäure mit einer durchschnittlichen Teilchengröße von 0,1 bis 100 nm in einer Menge von 5 bis 50 Gew.-%, bezogen auf den Feststoffgehalt im Überzug, und

(D) ein organisches Lösungsmittel vom Ketontyp in einer Menge von 40 Gew.-% oder mehr, bezogen auf den Überzug,

wobei der Feststoffgehalt im Überzug 10 bis 50 Gew.-% beträgt.